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Time-resolved magneto-optical Kerr effect for studies of phonon thermal transport

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Thanks to Brigit Hebler and Prof. Albrecht (Augsburg) for FePt: Cu samples; Dr. Hono (NIMS) for FePt: C samples; and André Kobs and Prof. Oepen (Hamburg) for Co/Pt films

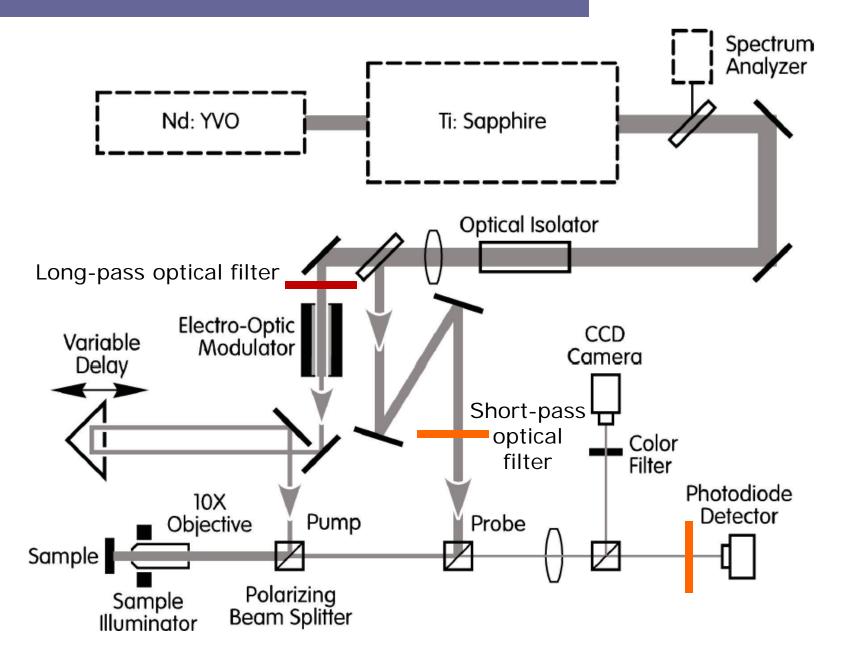
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Outline

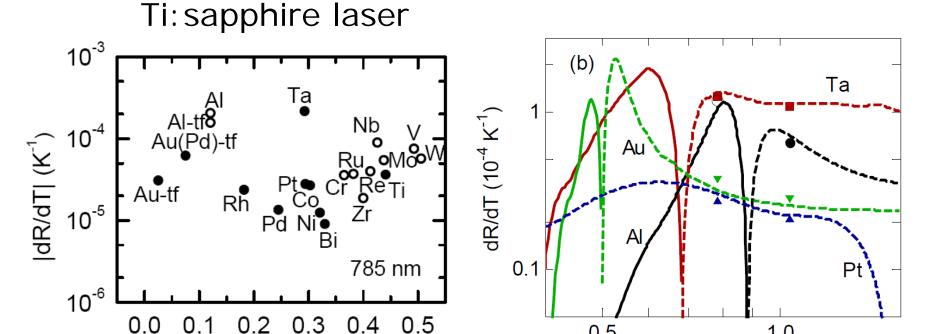
- Introduction to...
 - pump-probe measurements by conventional timedomain thermoreflectance (TDTR);
 - and time-resolved magneto-optic Kerr effect (TR-MOKE)
- Polarization signal generated by a magnetic layer enables use of thinner transducers
 - Less thermal mass → faster time resolution
 - Reduced in-plane thermal conductance
 - Greater sensitivity to interfacial phenomena when the Kapitza length is small
- Some practical issues of TR-MOKE versus TDTR
 - Ultrafast time response
 - Linearity and temperature range
 - Sensitivity and noise

Time-domain thermoreflectance



Large dR/dT is desired for higher signal-to-noise

R=optical reflectivity; T=temperature



Wang et al., JAP (2010)

1-R

Wilson et al., Optics Express (2012)

 $\lambda (\mu m)$

1.0

0.5

Thickness of the transducer sets limits on time-resolution

- Limited by interface conductance.
 - Equivalent to discharging of a capacitor through a resistor

$$\tau_G = \left(\frac{1}{AG}\right)(VC) = \frac{hC}{G}$$

$$h=60 \text{ nm}$$
; $C=2.5 \text{ MJ m}^{-3} \text{ K}^{-1}$; $G=200 \text{ MW m}^{-2} \text{ K}^{-1}$
 $\tau_G=0.75 \text{ ns}$

Thickness of the transducer sets limits on time-resolution

- Limited by effusivity of the sample
 - When does the heat capacity of a layer of the thermal diffusion distance in the sample equal the heat capacity of the metal film?

$$\left(\sqrt{D\tau_E}\right)C_s = hC_f$$
 $C_f \approx C_s = C;$ $\tau_E = \frac{h^2}{D}$

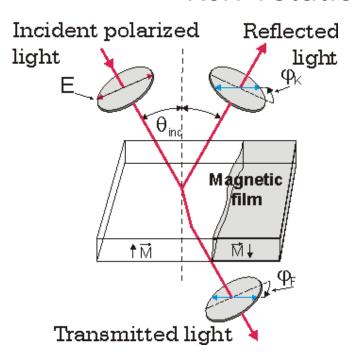
$$h = 60 \text{ nm}; \quad D > 10^{-7} \text{ m}^2 \text{ s}^{-1} \text{ (glassy polymer)}$$
 $\tau_E < 36 \text{ ns}$

What could we do if the transducer was 6 nm thick instead of 60 nm thick?

- Access time scales in high thermal conductivity crystals down at ~100 ps.
- Increase sensitivity to low thermal conductivity materials by reducing the product of modulation frequency (f = 10 MHz) and the cooling time of the transducer.
 - Even for a glassy polymer $2\pi f \tau_E \ll 1$
- Reduce parasitic in-plane thermal conductance of the metal film transducer, ultimately $h\Lambda_f\sim 0.1~\mu W~K^{-1}$
 - In our initial work using TR-MOKE, $h\Lambda_f=0.4~\mu\mathrm{W~K^{-1}}$ (vs. 10 $\mu\mathrm{W~K^{-1}}$ for Al in TDTR)

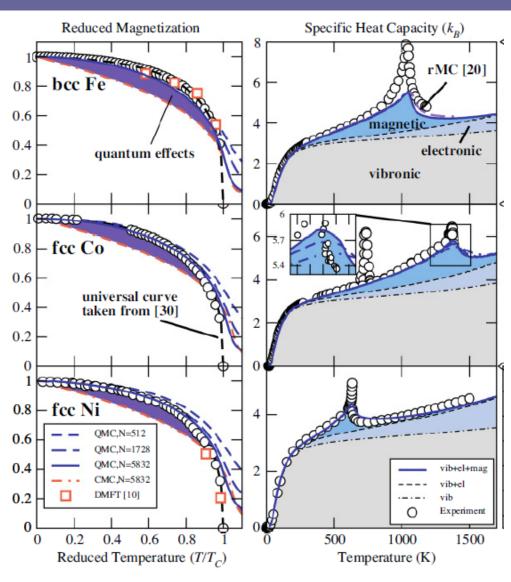
In TR-MOKE, dθ/dT replaces dR/dT of a conventional thermoreflectance measurement

Kerr rotation



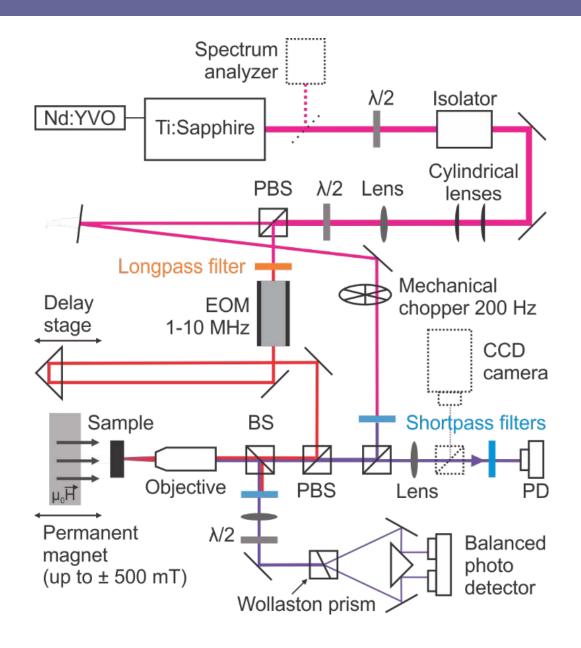
Faraday rotation

http://labfiz.uwb.edu.pl



Körmann et al., PRB (2011)

Time-resolved magneto-optic Kerr effect (TR-MOKE)



Perpendicular magnetic materials are the most convenient (polar Kerr effect)

• [Co,Pt] multilayers, 5-20 nm, sputter deposit at room temperature.

$$\frac{d\theta}{dT} \approx 10^{-5} \text{ K}^{-1}$$

 L1₀ phase FePt:Cu, 5 nm, sputter deposit at room temperature followed by rapid thermal annealing to 600 °C.

$$\frac{d\theta}{dT} \approx 8 \times 10^{-5} \text{ K}^{-1}$$

 Amorphous TbFe (Xiaojia Wang at UMN), 25 nm, sputter deposit, cap with Ta.

$$\frac{d\theta}{dT} \approx 3 \times 10^{-5} \text{ K}^{-1}$$

Kerr signal from a semitransparent magnetic layer is only weakly dependent on dn_s/dT of the sample

• For an optically thin magnetic transducer of thickness d, index n, and magneto-optic coefficient Q, on a sample of index n_s .

$$\theta = \frac{Qn^2}{\frac{\lambda}{4\pi d} \left(n_s^2 - 1\right) + i\left(n_s^2 - n^2\right)}$$

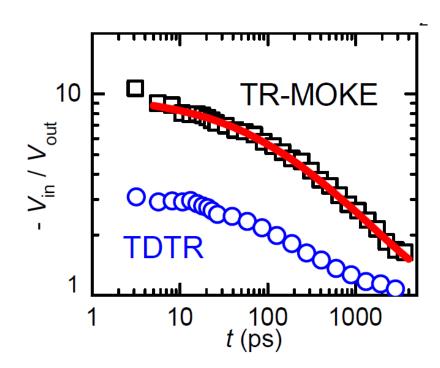
• The critical parameter entering into $\frac{d\theta}{dT}$ is

$$\left| \frac{1}{Q} \frac{dQ}{dT} \right| \sim 10^{-2} \text{ K}^{-1} \text{ for [Co,Pt]}$$

Kerr signal from a semitransparent magnetic layer is only weakly dependent on dn_s/dT of the sample

 Worst case scenario where laser excitation of the Si substrate creates a strong contribution to the TDTR signal. TR-MOKE is immune.

[Co,Pt](8 nm)/SiO₂(240 nm)/Si

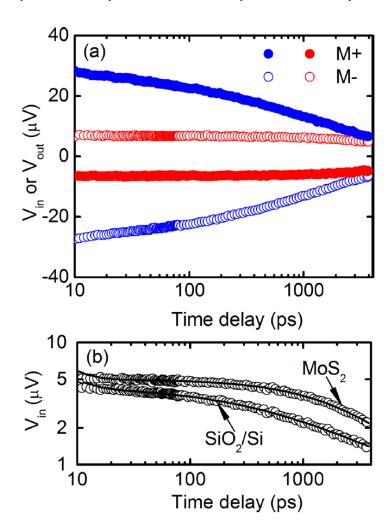


Our first application has been in measurements of inplane thermal conductivity

Pt/Co multilayers. Structure from top to bottom
 Pt(1 nm)/[Co(0.5 nm)Pt(1 nm)]×6/Pt(10 nm)

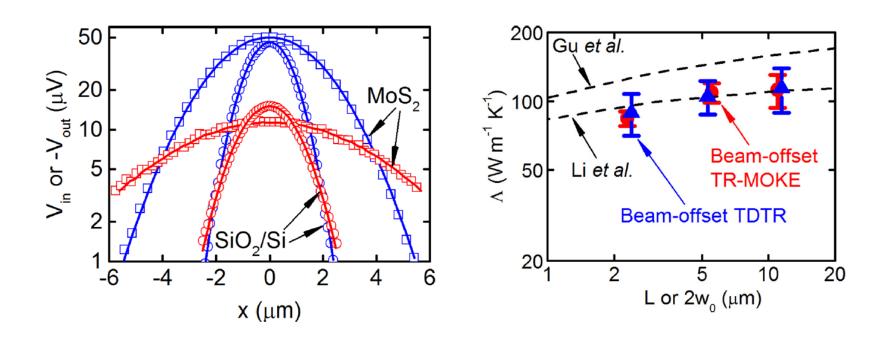
 Measurements are typically done for both orientations of the magnetization. Take difference to remove any residual thermoreflectance signal.

Liu et al., JAP (2014)



Our first application has been in measurements of inplane thermal conductivity: MoS₂

 Beam offset time-resolved MOKE measurements of [Co,Pt]/MoS₂ to determine in-plane thermal conductivity as a function of laser spot size.

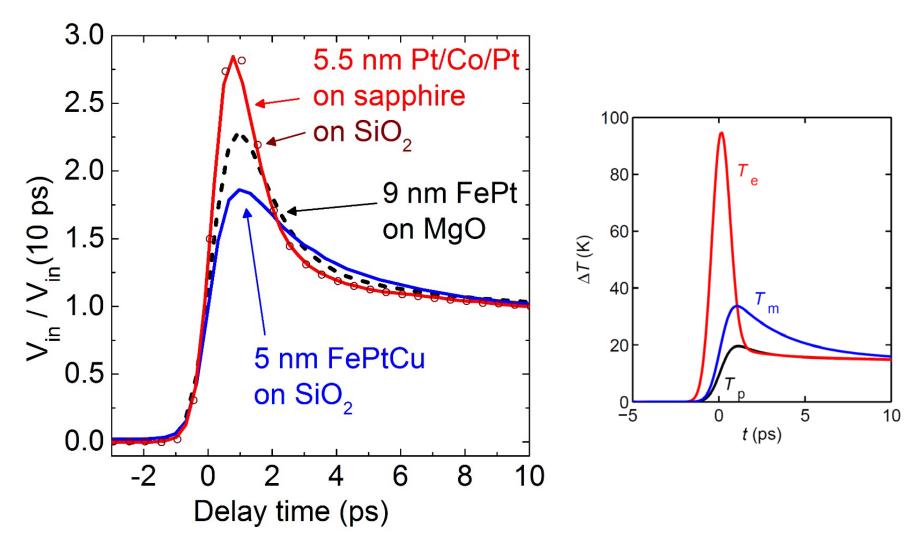


Liu et al., JAP (2014)

Dig into a few more technical details...

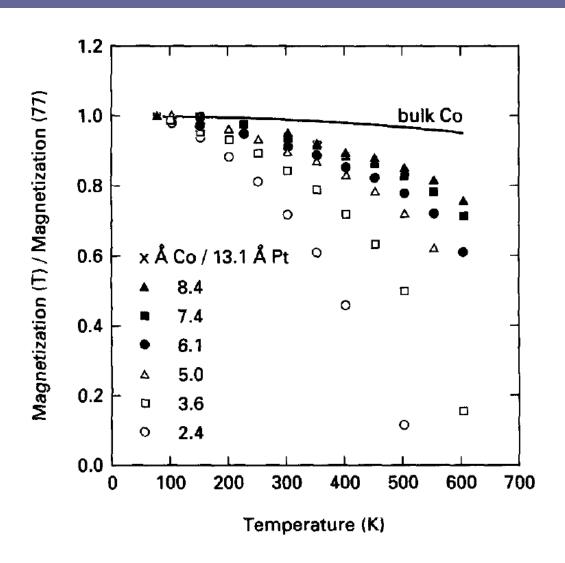
- Ultrafast time response
- Linearity and temperature range
- Sensitivity and noise

Magnetic transducers (far from T_c) have a time-response of a few ps governed by magnons \rightarrow electron \rightarrow phonon coupling



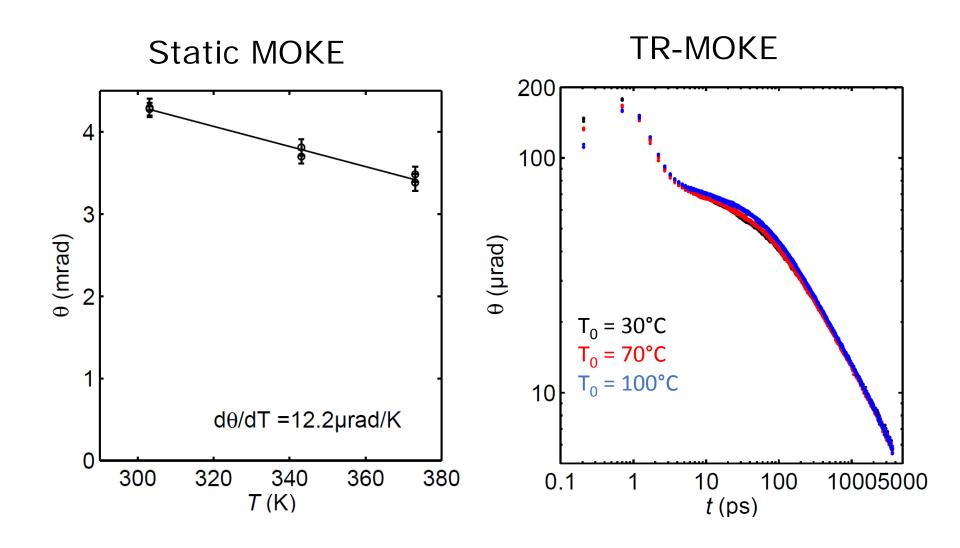
Kimling, PRB (2014)

Tradeoffs between sensitivity, linearity, and temperature range. Example of [Co,Pt] multilayers



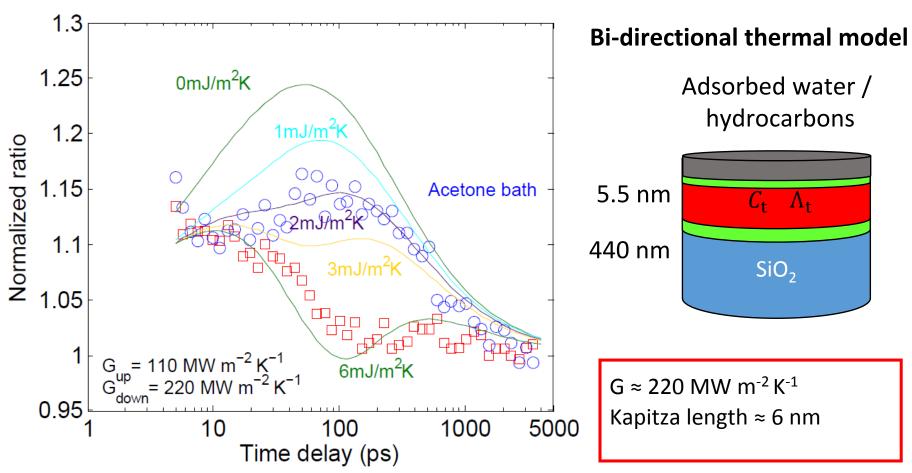
Kesteren and Zeper, JMMM (1993)

Single Co layer (0.8 nm thick) in the middle of 4 nm of Pt on 440 nm SiO₂/Si



Single Co layer (0.8 nm thick) in the middle of 4 nm of Pt on 440 nm SiO₂/Si

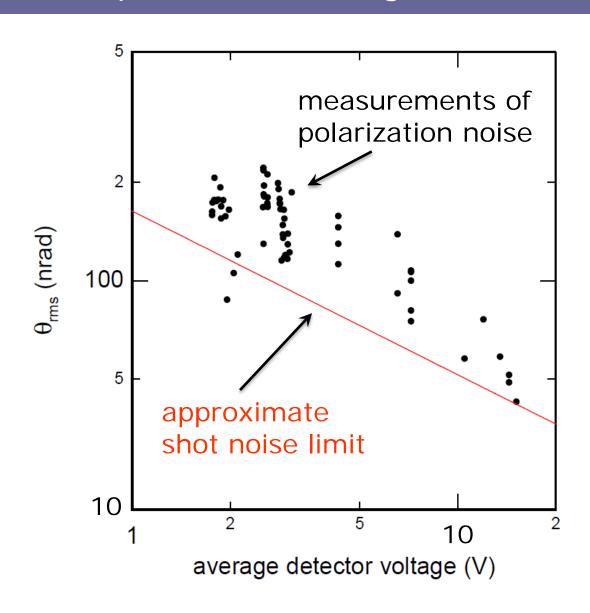
TR-MOKE data normalized to model with G = inf.



For comparison:

Areal heat capacity of 5.5 nm Co/Pt transducer: 16 mJ/m²K

Laser intensity noise is almost completely suppressed in a measurement of polarization using a balanced detector



Summary

- Thermoreflectance (thermometry by using intensity of light) versus magneto-optic Kerr effect (thermometry using polarization of light)
- Kerr effect transducers are relatively immune to what is happening in other parts of the sample. Polarization rotation is specific to the magnetic layer.
- Thin transducers enable higher time resolution and better sensitivity for in-plane transport.
- A single 0.8 nm layer of Co sandwiched in a 4 nm Pt layer provides high signal-to-noise and extremely small thermal mass. Need to find a simple way to control contamination by hydrocarbons and adsorbed water.
- Great opportunities for materials engineering of improved Kerr effect transducers to improve sensitivity and stability.